

FELDMAN Z. A.

Novocaine (procaine) block in lead poisoning Klinicheskaya Meditsina 1947, 1

4434 In 45 cases of oliguria, lead colic and other forms of entero-gastric dyskinesia, infiltration of the left perirenal tissues with 60 ml 0.5 per cent procaine gave gratifying results.

Van der Molen - Terwolde (SecVI)

SO: Section II Vol. 1<sup>2</sup> No. 7-12

TSEYTLIN, A.A.; FEL'DMAN, Z.D.; BUZNITSKIY, Ye.V.; DEKHTYAR, E.M.

Machine for making curvilinear reinforced concrete products. Suggested  
by A.A.TSeytlin, Z.D.Fel'dman, E.V.Buznitskii, E.M.Dekhtiar. Rats.  
i izobr. predl. v stroi. no.15:41-43 '60. (MIRA 13:9)

1. Po materialam Tekhnicheskogo upravleniya Ministerstva stroitel'stva  
USSR.

(Concrete panels)

Fel'dman, Z. b.  
KIRICHENKO, T.F.; FEL'DMAN, Z.G.

Record of trees and shrubs in the territory of the Veliko-Anadol'  
Forest. Nauk, zap. Dnpr. un. 48:227-239 '55 (MIRA 10:11) .  
(Ol'ginka District--Trees) (Ol'ginka District--Shrubs)

SANDLER, N.I.; DOBRUSKINA, Sh.R.; ZAYKOV, S.T.; FEL'DMAN, Z.N.; ASNIS, A.Ye.;  
NAZARENKO, A.N.

Converter low-alloys steel with niobium for welded structures.  
Avtom. svar. 17 no.2:43-48 F '64. (MIRA 17:9)

1. Ukrainskiy institut metallov (for Sandler, Dobruskina, Zaykov,  
Fel'dman). 2. Institut elektrosvarki im. Ye.O. Patona AN UkrSSR  
(for Asnis, Nazarenko).

FELDMAN, Z. YA.  
USSR/Microbiology - Antibiosis and Symbiosis. Antibiotics.

T-2

Abs Jour : Ref Zhur - Biol., No 5, 1958, 19433

Author : Feldman, Z. Ya.

Inst :

Title : Utilization of Antibiotics in Storing Lemon.

Orig Pub : Tr. Leningr. tekhnol. in-t kholodiln. prom-sti, 1956, 10, 72-73

Abstract : Antibiotic preparations were obtained by the method of N.V. Novotelnov from dog-rose fruit and bran. Antibiotics from bran were obtained with and without fermentation. These preparations when used with ascorbic acid exert high bactericidal properties, inhibit development of brown spots on lemons, and prevent spoilage of fruit to a considerable degree when it is stored at 13-15° for a period of 3 months. Most active was an antibiotic obtained from bran after fermentation. In its presence lemons were fully preserved at

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*Leningrad kholodil'nik. Glavnaya upravleniya  
gastronomicheskikh katekorynits magazinov*

Abs Jour : Ref Zhur - Biol., No 5, 1958, 19433

16-22° for a period of 2 months, while the majority of the control lemons became moldy after 10 days.

Card 2/2

SHVARTS, K. [Svaros, K.]; FELDMANE, E.

Microscopic studies of the defects in alkali-halogencous crystals by  
the evaporation method. Izv. AN Latv.SSR no.9:57-59 '63.

(MIRA 16:12)

1. Institut fiziki AN Latvyskoy SSR.

ACC NR: AP7005269

SOURCE CODE: UR/0371/66/000/006/0101/0102

AUTHOR: Kalnin, D. O.; Shavrts, K. K.; Feldmane, E. E.

ORG: Physics Institute, AN Latvian SSR (Institut fiziki AN LatvSSR)

TITLE: Dislocation density and radiation expansion in crystals

SOURCE: AN LatSSR. Izvestiya. Seriya fizicheskikh i tekhnicheskikh nauk, no. 6, 1966, 101-102

TOPIC TAGS: lithium fluoride, ~~radiation~~ <sup>crystal</sup> expansion, <sup>crystal</sup> dislocation, neutron irradiation, plastic deformation, crystal defect

ABSTRACT: Radiation expansion and point defects in crystals were studied experimentally. LiF crystals (10 x 10 x 2 mm) grown in a  $10^{-4}$  ton vacuum were used. Dislocation density, determined by  $\text{FeCl}_3$  etching, was  $10^4 \text{ cm}^{-2}$  for non-worked samples, and  $10^6 \text{ cm}^{-2}$  after plastic deformation at 1000K. The samples were irradiated with doses of  $4 \cdot 10^{14}$ — $4 \cdot 10^{17}$  neutrons/cm<sup>3</sup>. At low doses fractional volume expansion decreased slowly with increasing dislocation density; at high doses no effect was detected. The results indicate that an increase in dislocation density from  $10^4$  to  $10^6 \text{ cm}^{-2}$  has little effect on the radiation change in the volume in the range up to  $5 \times 10^{16}$  neutrons/cm<sup>3</sup>. This suggests that dislocations play an unimportant role in the crystal expansion. . Orig. art. has: 1 figure.

[JM]

SUB CODE: 20/ SUBM DATE: none/ ATD PRESS: 5115

Card 1/1

UDC: none

FEL'DMAN-BABAK, Tamara Petrovna; SURYGINA, E., red.; NEMCHENKO, I.,  
tekh.n.red.

[Outdoor swimming pools] Otkrytye iskusstvennyye basseiny dlia  
plavaniia. Kiev, Gos.isd-vo lit-ry po stroit. i arkhitekt. USSR,  
1960. 161 p. (MIRA 13:12)  
(Swimming pools)



**"APPROVED FOR RELEASE: Monday, July 31, 2000**

**CIA-RDP86-00513R000412830**

**APPROVED FOR RELEASE: Monday, July 31, 2000**

**CIA-RDP86-00513R000412830C**



FELDMANN, L. (Budapest, V., Szerb u.23)

On linear difference equations with constant coefficients. Periodica  
polytechn electr 3 no.3:247-257 '59. (EEAI 10:1)

1. Polytechnical University, Budapest.  
(Difference equations)

FEL'DMARK, Ya.

~~SECRET~~  
Nomogram for use in computing piston rings. Mor. i rech. flot 14 no. 4:  
25-26 Ap '54. (MLRA 7:5)  
(Piston rings)

FEL'DMUS, F.

Here we learn our trade. Mest.prom. i khud.promys. 4 no.4:  
23 Ap '63. (MIRA 16:10)

1. Direktor Golitsynskogo uchebnogo kombinata, Moskovskoy obl.

*FEL'DSHAU, A. F.*

**AUTHORS:** Fel'dshau, A.F. and Starokadomskiy, K. G. 65-1-14/14

**TITLE:** On a Source of Error During the Evaluation of Coals for Power Stations According to their Ash Content. (Ob odnom istochnike oshibok pri otsenke energeticheskikh ugley po ikh zol'nosti).

**PERIODICAL:** Khimiya i Tekhnologiya Topliv i Masel, 1958, No. 1, p. 72. (USSR).

**ABSTRACT:** The evaluation of coal on the basis of their ash content may lead to large errors when the mineral matter contains a considerable proportion of carbonates. Therefore, the best method of evaluation of coals for power generation is on the basis of their calorific value. The experiments were carried out by the Chemical Laboratory for Coal Investigations of the Lenin-Ugol' Trust of the Karagandaugol' Combine. A sample of coal was supplied by the No. 120 Trust of Saranugol:- specific weight = 1.83, ash content =  $A^a = 38\%$ , ash content of the dry mass  $A^s = 38.3\%$ ,  $CO_2^k = 23.6\%$ , calorific value  $Q^a = 3210$  kcal/kg (total fuel content  $Q^s = 5310$  kcal/kg). It is concluded that the ash content decreased by 23.6% and a value of  $Q^s = 8390$  kcal/kg is obtained which is near to the average value.

Card 1/1

**AVAILABLE:** Library of Congress.

INDENBAUM, I.S.; PERSHIN, G.N., prof., nauchnyy rukovod.; SEMILETOVA, A.,  
red.; FEL'DSHER, L., otv. za vypusk; SOYFERTIS, L., tekhn.red.

[Medicinal preparations; collection of annotations] Lekarstvennye  
preparaty; sbornik annotatsii. Pod nauchn.rukovodstvom G.N.  
Persheina. Sost. I.S.Indenbaum. Moskva, Kontora "Soyuzkhimfarm-  
torg," 1959. 332 p. (MIRA 13:3)

1. Russia (1923- U.S.S.R.) Glavnoye upravleniye mezhrespubli-  
kanskogo meditsinskogo snabzheniya i sbyta.  
(DRUGS)

POLYAKOV, N.G., prof.; CHERIKOVSKAYA, T.Ya., kand. med. nauk;  
SIDORKOV, A.M., kand. farmatsevt. nauk; BELEN'KIY,  
Ye.Ye., kand. med. nauk; KUZ'MINA, K.K., provizor;  
VASIL'YEVA, S.F., provizor; POLYAKOV, N.G., prof.,  
red.; FEL'DSHER, L.N., red.; KUCHERENKO, V.D., red.;  
CHULKOV, I.F., tekhn. red.

[Basic medicinal preparations and prepared drugs; a  
manual for physicians] Osnovnye lekarstvennye preparaty  
i gotovye formy; spravochnik dlia vrachei. Moskva,  
Medgiz, 1963. 359 p. (MIRA 17:2)

\*



POCHKOV, N.G., prof.; CHERIKOVSKAYA, T.Ya., kand. med. nauk;  
SIDORKOV, A.M., kand. farmatsevt. nauk; KUCHERENKO, V.D.,  
provizor; KUZ'MINA, K.K., provizor; VASIL'YEVA, S.F.,  
provizor; FEL'DSHER, L.N., provizor; ZAKOSHANSKIY, N.Ya.,  
red.

[Prepared drugs; a manual for physicians] Gotovye lekarst-  
vennye preparaty; spravochnik dlia vrachei. Moskva,  
Meditsina, 1965. 228 p. (MIRA 18:6)

ISMAILOV, I.M., inzh.; GAVRILENKO, I.V., kand.tekhn.nauk; Prinimali uchastiye:  
KUTYAVIN, S.M.; ORESHKIN, D.K.; TADZHIBAYEV, G.T.; AKHUNDZHANOV, A.I.;  
TONKIKH, P.I.; PANCHENKO, A.I.; FEL'DSHER, M.G.; VORONINA, L.D.

Lowering the solvent content in seed meal before treatment in evapor-  
ators. Matl.-zhir.prom. 26 no.10:7-13 O '60. (MIRA 13:10)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut zhirov (for Ismailov,  
Gavrilenko). 2. Uch-Kurganskiy masloekstraktsionnyy zavod (for Kutya-  
vin, Oreshkin, Tadzhibayev). 3. Sredneaziatskiy filial Vsesoyuznogo nauchno-  
issledovatel'skogo instituta zhirov (for Panchenko, Fel'dsher, Voronina).  
(Uch-Kurgan--Oil industries--Equipment and supplies)

DRUZHININ, I.G.; VARFOLOMEYEVA, L.T.; FEL'DSHER, S.A.

Comparative characteristics of the chemical composition of well  
waters on the "Vasil'evskii" State Farm. Uch. zap. Biol.-pochv.  
fak. Kir. un. no.7:155-162 '58. (MIRA 15:10)  
(Kirghizistan—Water—Composition)

MANT'YEV, V.A.; FEL'DSHEROV, I.A.

Analytical and micro-preparation apparatus for continuous paper electrophoresis. Vop. med. khim. 7 no.5:542-545 S-0 '61.

(MIRA 14:10)

1. The Biochemical Laboratory of the P.A.Gertsen State Oncological Institute, Moscow.

(PAPER ELECTROPHORESIS--EQUIPMENT AND SUPPLIES)

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**CIA-RDP86-00513R000412830C**

FEL'DSHON, V.

Our motto is mass participation! Voen. znar. 40 no.4:42  
Ap '64. (MTRA 17:6)

1. Zamestitel' predsedatelya fabrichnogo komiteta Vsesoyuznogo  
dobrovol'nogo obshchestva sodeystviya armii, aviatsii i flota  
SSSR po sportivnoy rabote, Kiyev.

GRIGOR'YEV, V. [Hryhor'iev, V.]; FEL'DSHON, Z., kand.tekhn.nauk; GINDIS, Ya. [Hindis, IA.], inzh.; AKININ, P., inzh.

Automation of the production of slag "pumice" on a centrifugal machine. Bud.mat.i konstr. no.5:22-25 S-0 '62. (MIRA 15:11)

1. Deystvitel'nyy chlen Akademii stroitel'stva i arkhitektury UkrSSR (for Grigor'yev).

(Automation control) (Slag)

	1ST AND 2ND ORDERS	PROCESSES AND PROPERTIES INDEX
FEL'DSHON, Z.D.		
CA		Continuous-action dialyzer for sugar industry. Z. D. Fel'dshon... U.S.S.R. 66,663, July 31, 1946. M. II.
		Patent: Purifying soln. [contg. sugar] (Inflico Inc.)
<b>A.S.T.M. METALLURGICAL LITERATURE CLASSIFICATION</b>		
A.S.T.M. SYMBOLS	SYMBOLS FOR CHEMISTRY	SYMBOLS FOR PHYSICS
GROUP NO.	SUBGROUP NO.	PROPERTY CODE

28



FEL'DSHON, Z.D.

Increasing the productivity of beet slicers. Sakh. prom. 31 no.6:22-  
23 Je '57. (MIRA 10:6)

(Sugar industry--Equipment and supplies)

FEL'DSHON, Z.D.

Continuous diffuser. Sakh.prom. 34 no.2:25-28 P '60.  
(MIRA 13:5)

(Sugar machinery) (Diffusers)

BRAND, V.E.; GRUTMAN, M.S. [Hrutman, M.S.]; FEL'DSHON, Z.D.; POLTORATSKAYA,  
Ye. [Poltorats'ka, E.], red.; IOAKIMIS, A., tekhn.red.

[Reed in rural construction] Komysh v sil's'komu budivnytstvi.  
Kyiv, Derzh.vyd-vo lit-ry s budivnytstva i arkhitektury URSS,  
1959. 122 p. (MIRA 14:2)  
(Reed (Botany)) (Farm buildings)

FEL'DSHTAYN, A.G.

On the treatment of hypertension. Sovet.med. no.4:30-31 Apr 51.  
(CML 20:8)

1. Candidate Medical Sciences Fel'dshtayn. 2. Odessa.

FEINBERG, A. I.

"Immunobiological displacements in persons who contacted with scarlet fever."

Zhur. Mikrobiol., Epidemiol., i Immunobiol., No. 6, 1944.

PHL'DSHTEYH, A.I.; GARZANOVA, G.V.

Variability of Gartner's bacillus; author's abstract. Zhur.  
mikrobiol.epid. i immun. 28 no.5:95-96 My '57. (MIRA 10:7)

1. Iz bakteriologicheskoy laboratorii Saratovskoy sanitarno-  
epidemiologicheskoy stantsii Stalinskogo rayona.  
(SALMONELLA ENTERITIDIS)

FEL'DSHTEN, A. L.

EA 1/50T37

USSR/Engineering - Transmission Lines Jul/Aug 49  
Radio - Transmission Lines

"Energy Relations in a High-Frequency Transmission Line," A. L. Fel'dshteyn, Engr, 5 pp

"Radiotekh" Vol IV, No 4

Discusses energy relations in a long line with losses for a fixed set of conditions at the terminus and starting point. Examines the conditions for optimal energy relations in treating the generator-line load system as a closed space. Introduces the concept of "operating quality" of such a system and the areas of application of this concept. Submitted 17 Mar 49.

1/50T37

FEL'DSTEYN, A. L.

"Matching of Transmission Lines", Radio, No 3, p 52, 1950.



RE: DSHTEYR, A. D.

Radiophysics, Application of Radiophysics Methods  
Radiotekhnika, Vol 6, No 5, 1951. "Nonuniform (Communications) Lines."

No abstract.

SO: Radiotekhnika, Vol 9, No 2, Mar/Apr 54; G-30785, 28 July 1954)

Radiophysics, Application of Radiophysics Methods  
Radiotekhnika, Vol 7, No 6, 1952. "Synthesis of Nonuniform (Communications) Lines."

No abstract.

SO: Radiotekhnika, Vol 9, No 2, Mar/Apr 54; (W-30785, 28 July 1954)

FEL'DSHTEYN, H. L.

5145. Non-uniform lines as filters. A. L. Fel'dsh'teyn. *Nachrichtentechnik*, 6, 284-8 (June, 1954). In German. An extension of the author's theory of symmetrical non-uniform lines (n.u.l.) [*Radiotekhnika*, 6, 1951]. A n.u.l. is inserted between two ordinary lines. In the lossless case, the filter action is described by the reflection coefficient of the n.u.l. An approximate expression for the reflection coefficient in the general case is given as an integral of a function of the wave resistance of the n.u.l. An advantage is that a filter with a given response can be synthesized by a Fourier transform method, characteristic points on the frequency axis of the response being related to the location of reflecting points along the length of the n.u.l. Good agreement is obtained between calculation and experiment for a simple filter consisting of a n.u.l. with sinusoidal length distribution of reflection.

S. C. DUNN

ST 340

AUTHORS: Fel'dshteyn, A. L., Member SOV/108-13-8-3/12  
of the Society

TITLE: Some Problems in the Synthesis of Heterogeneous Lines (Nekotoryye zadachi sinteza neodnorodnykh liniy)

PERIODICAL: Radiotekhnika, 1958, Vol. 13, Nr 8, pp. 13 - 23 (USSR)

ABSTRACT: The author describes the method of the synthesis by means of the Laplace integral and gives examples for the construction of heterogeneous lines according to given frequency characteristics. The approximation formula (10) of (Ref 1) serves as a basis for the calculation. This reference shows the connection between the line structure and the reflection factor at the line terminal: formula (1). The function given by formula (4) - which characterizes the relative change of the characteristic impedance is introduced and formula (1) is written down in the form of the transform according to Laplace-Karson (?) (Karson) as formula (5). The function  $F(p)$  occurring in it denotes the reflection factor and therefore can already previously be subjected to the limitations restricting the circuit functions that can be physically realized (Ref 2). These limitations are for the reflection factor the following: 1)  $|F(p)| \leq 1$  on the axis of real

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*Corres. Mbr. VNORIE*

Some Problems in the Synthesis of Heterogeneous Lines

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frequencies. 2)  $F(p)$ , besides the poles in the left semi-plane of the complex variable  $p$  does not have any other special points. The meromorphic function  $F(p)$  is then written down in form of a quotient of two integral functions and the final form for the equation (1) is obtained: formula (6). This integral equation has a general solution in form of the so-called expansion formula by Heaviside (Khevisayd): formulae (7) or (8). Examples are given. They show the use of the formulae (7) or (8). The examples can be divided into two groups: 1) The demanded frequency characteristic is given. 2) The equivalent circuit diagram LCR is given which is to be investigated. There are 14 figures and 4 references, 3 of which are Soviet.

SUBMITTED:

August 8, 1957

1. Frequency 2. Mathematics 3. Electric circuits

Card 2/2

SOV/109- -4-3-25/38

AUTHORS: Fel'dshteyn, A.L., Yavich, L.R.

TITLE: A Comparison of Step-like and Continuous Line Sections  
(K sravneniyu stupenchatykh i plavnykh perekhodov)

PERIODICAL: Radiotekhnika i Elektronika, Vol 4, Nr 3, 1959,  
pp 527-529 (USSR)

ABSTRACT: First, a Chebyshev-type step-like section (see Fig 1) is considered. This device was investigated by a number of authors (Refs 2,5,6 and 8). It is assumed that the length of this type of line section, which consists of  $n$  small steps is given by:

$$l_0 = \frac{1}{2\pi} \Lambda_2 n \arccos \left\{ \frac{1}{\cos \frac{K}{n}} \right\} \quad (1)$$

where  $\Lambda_2$  is the wavelength in the transmission line corresponding to the "long-wave" boundary of the transmission range;  $K$  is expressed by Eq (2), where  $R$  is the ratio between the characteristic impedances of the matched lines;  $h$  is the maximum deviation of the Chebyshev polynomial from its zero value. When  $n$  in Eq (1) tends to infinity, the line section represents a continuous transition, and Eq (1) is in the form of

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SOV/109- -4-3-25/38

A Comparison of Step-like and Continuous Line Sections

Eq (3). The problem consists of comparing values of  $l_0$ , as given by Eqs (1) and (3), for the same value of  $R$  and the same value of the reflection coefficient. The results are shown in Fig 4 for various values of  $n$  and  $\Gamma$ ; the limiting case of a continuous transition is represented by the dashed curves.

Card 2/2 There are 5 figures and 8 references, 6 of which are Soviet and 2 English. One of the Soviet references is translated from English.

SUBMITTED: September 18, 1958

report submitted for the Confidential Meeting of the Scientific Technological Society of  
Radio Engineering and Electrical Communications En. A. B. Popov (VSEEM), Moscow,  
6-12 June, 1959



69918

S/109/60/005/05/006/021  
E140/E435

9.1300

AUTHORS: Fel'dshteyn, A.L. and Yavich, L.R.  
TITLE: The Calculation of Stepped Junctions with Maximally-Flat Characteristics  
PERIODICAL: Radiotekhnika i elektronika, 1960, Vol 5, Nr 5, pp 762-770 (USSR)  
ABSTRACT: A method is given for calculating two- and three-step waveguide junctions with maximally-flat characteristics. Tables are given for wave-impedance changes between 1.2 and 9.2. Acknowledgements are expressed to R.Sh.Sharikova for her assistance with the calculation work. There are 9 figures, 2 tables and 3 Soviet references.

SUBMITTED: April 13, 1959

Card 1/1

9.1400

77175  
SOV/108-15-1-1/13

AUTHOR: Fel'dshteyn, A. L., Yavich, L. R.

TITLE: Engineering Computation of Chebyshev's Stepped Transitions

PERIODICAL: Radiotekhnika, 1960, Vol 15, Nr 1, pp 3-15 (USSR)

ABSTRACT: The paper is an exposition of the method of engineering computation of stepped transitions between transmission lines. The results of calculation of 405 typical problems are given in table form. The following two basic definitions are given: (1) A stepped transition is a quadrupole consisting of  $n$  sections of the transmission line ("steps") which have the same length  $l$  and various wave impedances  $\rho_1$  (see Fig. 1).

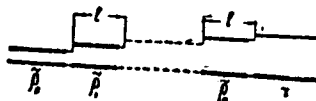


Fig. 1.

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Engineering Computation of Chebyshev's  
Stepped Transitions

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SOV/108-15-1-1/13

The purpose of a stepped transition is to match two lines with the wave impedances  $\rho_0$  and  $r$ , respectively. (2) A stepped transition is called optimal, or Chebyshev, when (a) for a selected wave impedance jump  $R = r/\rho_0$ , (b) a selected permissible mismatching value is  $|\Gamma|_{\max}$ , and (c) for a selected passband  $\lambda_2 - \lambda_1$ , the transition has a minimum overall length  $\ell_0 = n\ell$ . The attenuation of a Chebyshev transition equals  $10 \log_{10}$  of the magnitude  $|T_{11}|^2$ , which is:

$$|T_{11}|^2 = 1 + h^2 T_n^2\left(\frac{\cos \theta}{\rho}\right) = 1 + h^2 T_n^2(x), \quad (1)$$

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where  $T_{11}(x)$  is the Chebyshev polynomial of the first type and  $n$ -th order,  $n = 1, 2, 3 \dots$  being the

Engineering Computation of Chebyshev's  
Stepped Transitions

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SOV/108-15-1-1/13

number of transition steps;  $h$  is a parameter defining the permissible mismatch  $|\Gamma|_{\max}$ ;  $p$  is a parameter defining the width of the passband;  $\Theta = 2\pi Q/\Lambda$  is electrical length of the step and  $\Lambda$  is the wavelength in the transmission line. The stepped transitions are usually characterized by 5 parameters:  $n$ ,  $h$ ,  $p$ ,  $R$  and  $Q_0$ , of which 3 may be selected independently of each other whereas the two others follow from computation. The relationship between these parameters is derived from Eq. (1) by considering  $\cos \Theta = 1$ , i.e., for zero length of the steps, and taking values of the argument  $x = \cos \Theta/p$  at the boundaries of the passband. The following expressions have been obtained:

$$p = \frac{1}{\cos\left(\frac{1}{n} \arccos C\right)}. \quad (12)$$

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Engineering Computation of Chebyshev's  
Stepped Transitions

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$$\Lambda_1 = \frac{2\pi l}{\pi - \arccos p}, \quad (15)$$

$$\Lambda_2 = \frac{2\pi l}{\arccos p}, \quad (16)$$

where  $\Lambda_1$  and  $\Lambda_2$  are the wavelengths in the transmission line, generally different from  $\lambda_1$  and  $\lambda_2$  in the outside space. The length  $\ell_0 = n\ell$  is given as:

$$\frac{\ell_0}{\Lambda_2} = \frac{1}{2\pi} n \arccos \left( \frac{1}{\cos \frac{1}{n} \arccos C} \right), \quad (18)$$

Card 4/5

C in Eq. (18) and (12) is defined as:

Engineering Computation of Chebyshev's  
Stepped Transitions

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SOV/108-15-1-1/13

$$C = \frac{R-1}{2h\sqrt{R}}.$$

Expressions are given for the wave impedances  $\rho_1$  of the steps of transitions with  $n = 2$ ,  $n = 3$ , and  $n = 4$ . Values of  $R$ ,  $p$ , and  $\rho_1$  are given in tables for  $n = 2$ ,  $n = 3$ , and  $n = 4$ , and for various magnitudes of  $|\Gamma|_{\max}$ . The tables give the solution of 405 typical synthesis problems of stepped transitions. Two numerical examples illustrate the use of the tables for rapid computation of similar problems. In an appendix to the paper, expressions for  $\rho_1$  and  $\rho_2$  in a two-step transition are derived by comparing the coefficients of  $\cos \Theta$  in Eq. (1) and in an attenuation equation obtained as a product of matrices of stepped transition elements. R. Sh. Shakirova helped make the calculations.

Card 5/5

85722

9.1400(2703,3803,1006)

S/108/60/015/006/007/012/XX  
B010/B070

AUTHOR: Fel'dshteyn, A. L., Member of the Society  
TITLE: Generalized Matrix Theory<sup>10</sup> of Inhomogeneous Lines  
PERIODICAL: Radiotekhnika, 1960, Vol. 15, No. 6, pp. 10-17

TEXT: Systems of equations are given for the calculation of the elements of the transmission matrix of an inhomogeneous line. These equations appear promising for the unification of the methods of solving problems in line theory. It is assumed that the inhomogeneous line may be approximated by connecting numerous discreet passive four-poles in series. The transmission matrix (T) is, then, obtained as the product of the transmission matrices (T)<sub>i</sub> of the individual discreet four-poles. The following recurrence formulas hold for the elements (A<sub>k</sub>, B<sub>k</sub>, C<sub>k</sub>, D<sub>k</sub>) of the total matrix:

$$A_k = \prod_{i=1}^k a_i + \sum_{m=1}^k b_m C_{m-1} \prod_{i=m+1}^k a_i,$$

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Generalized Matrix Theory of Inhomogeneous Lines

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S/108/60/015/006/007/012/XX  
B010/B070

$$C_k = \sum_{m=1}^k c_m A_{m-1} \prod_{i=m+1}^k d_i, \quad B_k = \sum_{m=1}^k b_m D_{m-1} \prod_{i=m+1}^k a_i, \quad D_k = \prod_{i=1}^k d_i + \sum_{m=1}^k c_m B_{m-1} \prod_{i=m+1}^k d_i,$$

where  $a$ ,  $b$ ,  $c$ , and  $d$  are the matrix elements of the discrete four-poles, and  $k$  is their number. It is known that the wave transmission matrix  $a_1$ ,  $b_1$ ,  $c_1$ ,  $d_1$  of a section of line with wave impedance  $q_1$  and length  $\Delta x$  adjoining another section with the wave impedance  $q_{i+1}$  is given in the usual notation by the following relation:  $a_1 = \frac{1}{2} (\alpha_1 + 1/\alpha_1) e^{\gamma_1 \Delta x}$ ,  $b_1 = \frac{1}{2} (\alpha_1 - 1/\alpha_1) e^{-\gamma_1 \Delta x}$ , and similar expressions for  $c_1$  and  $d_1$ ,  $\alpha_1$  being  $\sqrt{(q_1 + 1)/q_1}$ .  $A_k$ ,  $B_k$ ,  $C_k$ , and  $D_k$  for discontinuous inhomogeneous lines may be calculated from the same expressions. For continuous inhomogeneous lines, that is, when the number of discrete four-poles becomes infinitely great, the sums and products go over into integrals:

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$$A(l) = \exp\left(\int_0^l \gamma(x)dx\right) + \int_0^l N(x)C(x)\exp\left(\int_x^l \gamma(x)dx\right)dx,$$

$$C(l) = \int_0^l N(x)A(x)\exp\left(-\int_x^l \gamma(x)dx\right)dx, \quad D(l) = \exp\left(-\int_0^l \gamma(x)dx\right) + \int_0^l N(x)B(x)$$

$$\exp\left(-\int_x^l \gamma(x)dx\right)dx, \quad B(l) = \int_0^l N(x)D(x)\exp\left(\int_x^l \gamma(x)dx\right)dx, \quad \text{where } N(x) = \frac{1}{2} \frac{d}{dx} \ln q(x),$$

$l$  is the length of the line; and  $A, B, C, D$  are elements of the transmission matrix. It is shown that these equations can be transformed, by the separation of variables, into four Volterra integral equations of the second degree which are known to yield well-converging series for the solution; also the error is easily estimated. The first approximation gives:

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$$A_1 = \exp\left(\int_0^1 \gamma(x) dx\right), B_1 = \exp\left(-\int_0^1 \gamma(x) dx\right) \int_0^1 N(x) \exp\left(2 \int_x^1 \gamma(x) dx\right) dx, \text{ and cor-}$$

responding expressions for  $C_1$  and  $D_1$ ; the magnitudes of the errors involved are given by  $\Delta A \leq (oh M1)^{-1}$ ,  $\Delta B \leq (sh M1) - M1$ , and corresponding expressions for  $\Delta C$  and  $\Delta D$ , where  $M = \max |N(x)|$  ( $0 \leq x \leq 1$ ). In some special cases, not dealt with in the paper, exact solutions may be obtained by solving the differential equations resulting from differentiating the integral equations with respect to the upper limit: ✓

$$\begin{aligned} A'' - (N'/N)A' - \{(\gamma^2 + N^2) + (\gamma' - \gamma N'/N)\} A &= 0, C'' - (N'/N)C - \{(\gamma^2 + N^2) \\ - (\gamma' - \gamma N'/N)\} C &= 0, B'' - (N'/N)B' - \{(\gamma^2 + N^2) + (\gamma' - \gamma N'/N)\} B &= 0, \\ D'' - (N'/N)D' - \{(\gamma^2 + N^2) - (\gamma' - \gamma N'/N)\} D &= 0, \end{aligned}$$

where  $A, B, C, D$  are the transmission matrix elements, and the primed quantities are differential coefficients with respect to  $l$ . In conclusion, it is indicated that the

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B010/B070

difficult calculation of the input reflection coefficient may be simplified with the help of Riccati's differential equation combined with the solutions of the four integral or differential equations. There are 4 figures and 12 Soviet references.

SUBMITTED: December 17, 1958

X

Card 5/5

FEL'DSHTEYN, A.L.

Use of network theory methods in the synthesis of systems with distributed constants. Radiotekhnika 15 no.11:11-22 N '60.

(MIRA 13:11)

1. Deystvitel'nyy chlen Nauchno-tekhnicheskogo obshchestva radiotekhniki i elektrosvyazi imeni A.S.Popova,  
(Electric networks)

9,1900 (also 2603)

20577

S/109/61/006/002/009/023  
E140/E435

AUTHOR: Fel'dshteyn, A.L.

TITLE: The Synthesis of Step Directional Couplers

PERIODICAL: Radiotekhnika i elektronika, 1961, Vol.6, No.2,  
pp.234-240

TEXT: The author starts from the well-known directional coupling properties of coupled homogeneous transmission lines. Relationships are developed for two special cases: 1) directional couplers with minimum number of sections (Chebyshev or isoextremal characteristics); 2) coupler with maximally-smooth characteristics. The author also considers the question of the physically attainable properties of directional systems. The analysis proceeds from the single-step directional coupler (homogeneous symmetrical coupled lines), multi-step directional coupler (cascade connection of arbitrary number of homogeneous coupled lines) and the limiting case of the multi-step system (inhomogeneous coupled lines). It is found that the last case presents an infinite passband dropping to zero only at zero frequency. The division of power between the branches has a polynomial character, permitting the design of directional couplers with similar

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The Synthesis of Step ...

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properties to those of step tapers and step filters. Certain mathematical demonstrations are included in an appendix. There are 6 figures, 1 table and 9 references: 8 Soviet and 1 English.

SUBMITTED: June 9, 1960

X

Card 2/2

FEL'DSHTEYN, A.L.

Step bridges. Radiotekh. 1 elektron. 6 no.9:1581-1582 S '61.  
(Radio lines) (MIRA 14:8)

22728

S/108/61/016/005/002/005  
B104/B205

9,1400  
AUTHOR:

Fel'dshteyn, A. L., Member of the Scientific and Technical  
Society of Radio Engineering and Electric Communications  
imeni A. S. Popov

TITLE:

Non-uniform coupled lines

PERIODICAL: Radiotekhnika, v. 16, no. 5, 1961, 7. - 14

TEXT: It is first noted that there are no data available in the literature on the theory of non-uniform coupled lines, which offers new possibilities for the synthesis of optimum superhigh-frequency eight-terminal networks. In presenting this theory, the author proceeds from a network consisting of a cascade-connected eight-terminal networks which he considers to be composed of two eight-terminal networks, i.e., the  $s$ -th eight-terminal network and the system of the preceding  $(s-1)$  eight-terminal networks. Therefore, the transmission matrix of the entire system may be represented as the product of the transmission matrix of the  $s$ -th eight-terminal network and that of the system of  $(s-1)$  eight-terminal networks. Based on these assumptions, the author obtains four systems of equations describing the network of a eight-terminal networks with  
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discretely varying parameters. Next, a network is studied, in which each eight-terminal network is considered to be a pair of symmetric homogeneous lines (Fig. 2). The cascade connection of these lines is regarded as a coupled line of several stages (Fig. 3). Current and voltage in homogeneous, coupled lines are known to be given by the system

$$\left. \begin{aligned} U_1 &= U_2 \cos ml + j(\rho I_2 + r I_1) \sin ml \\ U_2 &= U_1 \cos ml + j(r I_1 + \rho I_2) \sin ml \\ I_1 &= I_2 \cos ml + j\left(\frac{U_2}{w} - \frac{U_1}{v}\right) \sin ml \\ I_2 &= I_1 \cos ml + j\left(\frac{U_1}{w} - \frac{U_2}{v}\right) \sin ml \end{aligned} \right\} \quad (13)$$

where  $\rho$  and  $w$  stand for the characteristic impedance, and  $r$  and  $v$  for the coupling impedance. The coefficients of Eqs. (13) form the matrix

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$$[a] = \begin{bmatrix} \cos \theta & 0 & i \rho \sin \theta & i r \sin \theta \\ 0 & \cos \theta & i r \sin \theta & i \rho \sin \theta \\ \frac{i \sin \theta}{w} & -\frac{i \sin \theta}{v} & \cos \theta & 0 \\ -\frac{i \sin \theta}{v} & \frac{i \sin \theta}{w} & 0 & \cos \theta \end{bmatrix} \quad (15)$$

of the stages. From this matrix one obtains the wave-transmission matrix

$$[T] = \begin{bmatrix} A & 0 & 0 & -M \\ 0 & A & -M & 0 \\ 0 & M & A^* & 0 \\ M & 0 & 0 & A^* \end{bmatrix} =$$

$$= \begin{bmatrix} \cos \theta + i \rho \sin \theta & 0 & 0 & -i r \sin \theta \\ 0 & \cos \theta + i \rho \sin \theta & -i r \sin \theta & 0 \\ 0 & i r \sin \theta & \cos \theta - i \rho \sin \theta & 0 \\ i r \sin \theta & 0 & 0 & \cos \theta - i \rho \sin \theta \end{bmatrix} \quad (18)$$

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Non-uniform coupled lines

of the stages on the assumption that all lines in the eight-terminal network have the same characteristic impedance ( $\rho_1 = \rho_2 = \rho_3 = \rho_4 = R$ ) and the condition  $rv = R^2$  is satisfied. Here,  $r \sim r/R$  and  $\rho \sim \rho/R$  are normalized. This system is fully determined by the two elements A and M, for which the following relations are derived by passing to a limit. In this procedure, the entire system is conserved and the number of stages is infinitely increased:

$$A(l) = \exp\left(\text{im} \int_0^1 \rho(x) dx\right) - \text{im} \int_0^1 r(x) M(x) \exp\left(\text{im} \int_x^1 \rho(x) dx\right) dx \quad (22)$$

$$M(l) = \text{im} \int_0^1 r(x) A(x) \exp\left(-\text{im} \int_0^x \rho(x) dx\right) dx \quad (23)$$

Thus, non-uniform coupled lines with balanced current and voltage coupling are fully determined by two integral equations similar to those obtained for non-uniform single lines. The successive approximation of Eqs. (22) and (23) and design problems are discussed finally. It is shown that of the four parameters ( $\rho$ ,  $w$ ,  $r$ ,  $v$ ) of coupled double conductors, only two parameters, e.g.,  $\rho$  and  $r$ , are independent. An additional coupling,

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$rv - R^2 = 1$ , exists in the case under consideration (Fig. 4). Hence, only one of the four parameters is independent, e. g.,  $r(x)$  which is then given by the relation  $r(x) = 60 \ln \left\{ 1 + \left( \frac{D}{a_{12}} \right)^2 \right\}$ . It is shown that, if the coupling impedance in this form can be changed by a change of  $D$ , the relation  $\varphi(x) = \sqrt{1+r^2(x)} = 120 \ln \frac{D}{a}$  will be obtained only by varying the diameter  $a$  of the conductor. If  $r(x)$  is obtained by varying  $a_{12}$ , then the corresponding change of  $\varphi(x)$  will be brought about through a variation of  $D$  or  $a$ . Similar results are obtained for lines with coaxial or plane coupling. There are 4 figures and 6 Soviet-bloc references.

SUBMITTED: October 10, 1960

Card 5/6

FEL'DSHTEYN, A.L.

Methods for solving summative equations. Radiotekhnika 16 no.6:38-39  
Je '61. (MIRA 14:6)

1. Deyatvitel'nyy chlen Nauchno-tehnicheskogo obshchestva  
radiotekhniki i elektrosvyazi.

(Integral equations)

(Matrices)

(Electric networks)

33778

S/108/62/017/001/005/007

D271/D304

9,1300

AUTHORS: Fel'dshteyn, A.L., and Zhavoronkova, Ye.S., Members of the Society (see Association)

TITLE: Calculating the Chebyshev directional couplers, with loose coupling

PERIODICAL: Radiotekhnika, v. 17, no. 1, 1962, 40 - 50

TEXT: A synthesis method is presented for multi-element optimal directional couplers, and design data are tabulated for couplers consisting of 2 - 11 elements. The coupler which is considered is shown in Fig. 2; its function is to branch a required power from the main line 1-3 into 4, while the leak into 2 remains below the permitted limit. Transfer coefficients  $S_{12}$  and  $S_{14}$  are functions of frequency; if they are of Chebyshev (iso-thermal) character, a minimum number of elements is required. Elements of the coupler are four-port networks as shown in Fig. 3, where  $\alpha$  is the number of the element. Scatter matrices of the coupler and of its elements are of the type

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Calculating the Chebyshev directional ... D271/D304

$$[S] = \begin{bmatrix} S_{11}S_{12} & S_{12}S_{14} \\ S_{12}S_{11} & S_{14}S_{12} \\ S_{12}S_{14} & S_{11}S_{12} \\ S_{14}S_{12} & S_{12}S_{11} \end{bmatrix} \quad \text{and} \quad [S]_a = \begin{bmatrix} S_{11}^* & S_{12}^* & S_{13}^* & S_{14}^* \\ S_{12}^* & S_{11}^* & S_{14}^* & S_{13}^* \\ S_{13}^* & S_{14}^* & S_{11}^* & S_{12}^* \\ S_{14}^* & S_{13}^* & S_{12}^* & S_{11}^* \end{bmatrix} \quad (1)$$

Wave transfer matrix  $[T]_a$ , assuming  $S_{11}, S_{13}, S_{14} \ll 1$  and  $S_{12} \cong 1$ , is

$$[T]_a = \begin{bmatrix} e^{i\theta} & -S_{14}^* e^{i\theta} & -S_{11}^* & -S_{12}^* \\ -S_{14}^* e^{i\theta} & e^{i\theta} & -S_{12}^* & -S_{11}^* \\ S_{11}^* & S_{12}^* & e^{-i\theta} & S_{14}^* e^{-i\theta} \\ S_{12}^* & S_{11}^* & S_{14}^* e^{-i\theta} & e^{-i\theta} \end{bmatrix} \quad (8)$$

where  $\theta = \frac{2\pi l}{\Delta}$ . Transfer coefficients are then written out as  
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Calculating the Chebyshev directional... S/108/62/017/001/005/007  
D271/D304

$$S_{11} = e^{-1\theta} \sum_{\alpha=1}^n S_{11}^{\alpha} e^{-12(n-\alpha)\theta}, \quad (9) \quad S_{13} = \prod_{q=1}^n S_{13}^{\alpha} e^{-1\theta} \approx e^{-1n\theta}, \quad (11)$$

$$S_{12} = e^{-1\theta} \sum_{\alpha=1}^n S_{12}^{\alpha} e^{-12(n-\alpha)\theta}, \quad (10) \quad S_{14} = e^{-1n\theta} \sum_{\alpha=1}^n S_{14}^{\alpha}, \quad (12)$$

where each parameter of the coupler depends only on element parameters of the same designation. A particular case is considered when an element of the coupler is non-directional; because of symmetry

$$-S_{11}^{\alpha} = S_{12}^{\alpha} = S_{14}^{\alpha} = 1C_{\alpha} \quad (13)$$

where  $10 \log \frac{1}{C_{\alpha}^2}$  is transfer attenuation of one element. Transfer coefficients  $S_{12}$  and  $S_{14}$  become

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Calculating the Chebyshev directional... S/108/62/017/001/005/007  
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$$S_{12} = \sum_{\alpha=1}^n C_{\alpha} e^{-12(n-\alpha)\theta} \quad (14)$$

$$S_{14} = \sum_{\alpha=1}^n C_{\alpha} \quad (15)$$

The entire system is then fully determined by values of  $C_{\alpha}$ ,  $S_{12}$  is a Fourier series which may be transformed into Chebyshev polynomials. The maximum value of  $S_{12}$  is equal to  $S_{14}$ ;  $S_{14}$  is independent of frequency if  $C_{\alpha}$  does not depend on frequency. This last property permits one to optimize the entire system by bringing only  $S_{12}$  into the form of Chebyshev polynomial. Expressions are obtained from (14) for various values of  $n$ , e.g. for  $n = 4$ :

$$S_{12} = (2C_1 \cos 3\theta + 2C_2 \cos \theta) e^{-13\theta}, \quad (C_1 = C_4; C_2 = C_3). \quad (19)$$

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Calculating the Chebyshev directional... S/108/62/017/001/005/007  
D271/D304

It is postulated that backward transfer coefficient determined by expressions as above must have Chebyshev frequency characteristics:

$$|S_{12}|_n = h T_{n-1} \left( \frac{\cos \theta}{p} \right), \quad (21)$$

where  $h$  and  $p$  are amplitude and scale coefficients,  $T_{n-1}(\Omega)$  - Chebyshev polynomial of first class and  $(n-1)$  order;  $h$  represents permitted value of  $S_{12}$  in the coupler pass-band. The obtainable value of  $p$  is

$$p = \frac{1}{\operatorname{ch} \left[ \frac{1}{n-1} \operatorname{ar ch} \sqrt{k} \right]}, \quad (24)$$

where  $k$  is the minimum prescribed directivity;  $k = |S_{14}|^2/h^2$ . When  $p$  is known, the required number of elements can be found from

$$n = \frac{\operatorname{ar ch} \sqrt{k}}{\operatorname{ar ch} \frac{1}{p}} + 1. \quad (25)$$

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Calculating the Chebyshev directional... S/108/62/017/001/005/007  
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In design work it is not  $p$  which is of interest but the working range  $\Delta = 2 \frac{\lambda_2 - \lambda_1}{\lambda_2 + \lambda_1}$  and overlap coefficient  $\chi = \lambda_2/\lambda_1$ , which are obtained from  $p$ . In order to determine transfer coefficients of elements  $C_1, C_2$ , etc., Chebyshev polynomials are transformed into a form similar to that of the expression (19), e.g.

$$T_4\left(\frac{\cos \theta}{p}\right) = \frac{1}{p^4} \cos 4\theta + 4\left(\frac{1}{p^4} - \frac{1}{p^2}\right) \cos 2\theta + \left(\frac{3}{p^4} - \frac{4}{p^2} + 1\right). \quad (32)$$

By comparing expressions of the type (19) and (32) values of  $C_n/h$  are obtained as a function of  $p$ . These are tabulated (in dB) in design tables. Diameters of coupling holes are determined for the case of a coupler formed by two identical waveguides coupled by circular holes in the common short wall. For loose coupling, the expression relating transfer attenuation to dimensions of the hole is

$$L_{dB} = 20 \log \frac{1}{C_1} = 20 \log \frac{12 b}{\pi \Delta} \left(\frac{a}{d}\right)^3. \quad (34)$$

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Calculating the Chebyshev directional... S/108/62/017/001/005/007  
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A numerical example is given illustrating the application of the method. Design data are presented in 10 tables giving values for  $n = 2, 3, \dots, 11$  and  $p = 0.1, 0.2, \dots, 1.0$ . There are 6 figures, 10 tables and 10 references: 5 Soviet-bloc and 5 non-Soviet-bloc. The 4 most recent references to the English-language publications read as follows: W.R. Hewlett, U.S.A. patent specification 2,871,452 of January 27, 1959; E. Hensperger, The microwave journal, issue 2, no. 8, 1959; B. Levy, Proc. I.E.E., part C, no. 337E, 1959; J. Reed and G.J. Wheeler, I.R.E. transactions on microwave theory and techniques. MTT-4, no. 4, 1956.

ASSOCIATION: Nauchno-tekhnicheskoye obshchestvo radiotekhniki i elektrosvyazi im. A.S. Popova (Scientific and Technical Society of Radio Engineering and Electrical Communications imeni A.S. Popov) [Abstractor's note: Name of association taken from first page of journal]

SUBMITTED: October 26, 1960

Card 7/87

FEL'DSHTEYN, Aleksandr L'vovich; YAVICH, Lev Rafaelovich; SMIRNOV,  
Vitaliy Petrovich; PERETS, R.I., red.; BUL'DYAYEV, N.A.,  
tekhn. red.

[Manual on the elements of waveguide technology] Spravochnik  
po elementam volnovodnoi tekhniki. Moskva, Gosenergoizdat,  
1963. 359 p. (MIRA 17:2)

FEL'DSHTEYN, A.L.; SMIRNOV, V.P.

Characteristic impedance of a rectangular wave guide. Radiotekhnika  
18 no.4:78 Ap '63. (MIRA 16:5)

1, Deystvitel'nyy chlen Nauchno-tekhnicheskogo obshchestva  
radiotekhniki i elektrosvyazi imeni Popova.  
(Wave guides)

~~L 10107-63~~ BDS  
ACCESSION NR: AP3001124

S/0108/63/018/006/0015/0025

45

AUTHOR: Mazepova, O. I.; Fal'dshteyn, A. L.; Yavich, L. R. Members of the Society  
(see Association)

TITLE: Engineering calculation of SHF band-pass filters

SOURCE: Radiotekhnika, v. 18, no. 6, 1963, 15-25

TOPIC TAGS: SHF band-pass filter

ABSTRACT: The method of SHF filter calculation is based on an equivalent replacing of the lumped-parameter systems (low-pass filters and ladder-type band-pass filters) with the filters formed by inhomogeneities in waveguides. The article offers: (1) a systematic procedure for calculating SHF filters with quarter-wave couplings; (2) tabulated typical calculations. Functions of effective attenuation for both the Tchebycheff and the maximum-flat-frequency response filters are evaluated. Cavity resonators are represented by waveguide stubs terminated with three inductive posts on each end. The design tables were compiled by means of an electronic computer. "Programing was performed by Engineer A. V. Ivakina." Orig. art. has: 9 formulas, 11 figures, and 7 tables.

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L 10407-63

ACCESSION NR: AP3001124

ASSOCIATION: Nauchno-tehnicheskoye obshchestvo radiotekhniki i elektrosvyazi im  
A. S. Popova (Scientific and Technical Society of Radio Engineering and Electro-  
communications)

SUBMITTED: 07 Aug62

DATE ACQD: 01Jul63

ENCL: 00

SUB CODE: CO,SD

NO REF SOV: 002

OTHER: 006

Ja/ps  
Card 2/2



ACCESSION NR: AP4042891

S/0108/64/019/007/0033/0038

AUTHOR: Fel'dshteyn, A. L. (Active member)

TITLE: Nonreciprocal nonuniform lines

SOURCE: Radiotekhnika, v. 19, no. 7, 1964, 33-38

TOPIC TAGS: nonuniform line, nonreciprocal line, nonreciprocal line theory

ABSTRACT: A long line with continuously varying (in the direction of propagation) nonreciprocal parameters is called a "nonreciprocal nonuniform line." In such a line, the attenuation and phase shift depend on the direction of transmission (ferrite, plasma, etc.). By considering the line as a ladder of quadripoles and by separating the reciprocal part from the nonreciprocal in each section, a theory of such lines is developed. The reciprocal part of a section is characterized by the half-sum of the conventional propagation constants  $\gamma_1(x)$  and  $\gamma_2(x)$ , while the nonreciprocal part is characterized by their half-difference. The integrals of

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ACCESSION NR: AP4042891

these quantities enter the formulas describing the line. Integral and differential formulas for the matrices of transmission and dissipation of the line are developed. "The author wishes to thank V. G. Kalina for discussing the results of the work." Orig. art. has: 1 figure and 30 formulas.

ASSOCIATION: Nauchno-tekhnicheskoye obshchestvo radiotekhniki i elektrosvyazi  
(Scientific and Technical Society of Radio Engineering and Electrocommunication)

SUBMITTED: 07Feb63

ENCL: 00

SUB CODE: E0

NO REF SOV: 004

OTHER: 000

Card 2/2

FEL'DSHTYN... Aleksandr L'vovich; YAVICH, Lev Rafnelovich. Pri-  
nimala uchastiye PROKHOROVA, N.I.; YAKOBSON, A.Kh.

[Synthesis of four-terminal and eight-terminal micro-  
wave networks] Sintez chetyrekhpoliusnikov i vos'mipo-  
liusnikov na SVCh. Moskva, Izd-vo "Sviaz'," 1965. 352 p.  
(MIRA 18:5)

L 26415-66 EWA(h)/EWT(1)

ACC NR: AM5018516

Monograph

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60  
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Fel'dshteyn, Aleksandr L'vovich; Yavich, Lev Rafaelovich

Synthesis-high frequency four-terminal and eight-terminal networks /  
chetyrekhpol'yusnikov i vos'mipol'yusnikov na SVCh) Moscow, Izd-vo "Svyaz" , 1965.  
352 p. illus., biblio. 5700 copies printed.

TOPIC TAGS: communication network, array synthesis, superhigh frequency, SHF communi-  
cation, transmission line, waveguide coupler

PURPOSE AND COVERAGE: This book is intended as a manual for scientists, technicians,  
and college students concerned with the theory and operation of transmission lines.  
Theoretical and design problems concerning filters, matching devices, directional  
couplers, and other similar devices. The authors thank O. I. Masepova, Ye. V.  
Solov'yeva, A. V. Ivakina, V. P. Smirnov, R. Sh. Shakirova, and N. I. Prokhorova  
for their assistance.

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Ch. II. External wave parameters of four-terminal networks -- 31

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UDC: 621.372.5/6:621.3.029.6.001.24

L 26415-66

ACC NR: AM5018516

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  - Ch. V. Matrix theory of heterogeneous lines with continuously varying parameters -- 100
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SUB CODE: 09/ SUBM DATE: 09Apr65/ ORIG REF: 080/ OTH REF: 033

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Reviews classical methods which entirely reproduce the corresponding type of machining, accelerated methods of investigation based on short-time tests, and the relation between mechanical properties of metals and their workability. Emphasis is on "face machining"; and experimental verification of applicability of this method is presented. 75 ref. (G17, Q23)

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Marshall Sittig



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Comments and Evaluation B-78524, 8 Sep 54

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Obrabatyvaemost' stalei pri skorostnom rezanii. (Vestn. Mash., 1950, no. 9, p. 43-48) Includes bibliography.

Machinability of steel during high-speed cutting.

DLC: TN4.V4

SO: Manufacturing and Mechanical Engineering in the Soviet Union, Library of Congress, 1953.

EXTRACT AND INDEX										PROCESSES AND PROPERTIES INDEX										EXTRACT AND INDEX									
3																				5									
<p>4791* Fundamentals of Processes for Rapid Cutting of Steels. (In Russian.) E. I. Fekhtel'man. <i>Stanki i Instrumenty</i> (Machine Tools and Equipment), v. 21, Dec. 1960, p. 13-19. Results of experimental investigation indicate existence of errors in previous theories of the above, and clarify basic factors affecting tool stability during rapid cutting, which depends on microstructure. Imparting a pearlite structure to medium- and high-carbon steels was found to be effective in improving their machinability. 13 ref.</p>																													
<p>AS 6-51A METALLURGICAL LITERATURE CLASSIFICATION</p>																													
<p>EXTRACT AND INDEX</p>																													

PHASE I

TREASURY ISLAND BIBLIOGRAPHICAL REPORT

AID 482-1

BOOK

Call No.: AF639674

Authors: BASOV, M. I., Kand. of Tech. Sci., FEL'DSHTEYN, E. I., Kand.  
of Tech. Sci., BRAKHMAN, I. A., Eng., STICHAYEV, YA. F., Eng.,  
KRYSSINA, YE. V., Eng., BOL'SHAKOV, V. M., Tech., BYCHKOV, P. P.,  
Eng., BARYLOV, G. I.

Full Title: CUTTING TOOLS WITH HARD-ALLOY MULTIPLE BLADE INSERTS

Transliterated Title: Rezhushchiye instrumenty s mnogolezviynymi  
vstavkami iz tverdogo splava

PUBLISHING DATA

Originating Agency: None

Publishing House: State Scientific and Technical Publishing House of  
Machine-Building Literature (Mashgiz)

Date: 1952

No. pp.: 110

No of copies: 8,000

Editorial Staff

Editor: Basov, M. I., Kand. of Tech. Sci.

TEXT DATA

Coverage: This monograph is the collective work of authors from the  
Institute of the Organization of the Automobile Industry, the Gor'kiy  
Automobile Plant im. Molotov (ZIM) and the Moscow Automobile Plant im.  
Stalin (ZIS). The authors describe the designs of modern cutting tools  
with hard-alloy multiple blade inserts, the results of their study and  
experience with the tools' cutting properties, and the advantages of

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Razhushchiye instrumenty s mnogolezviynymi  
vstavkami iz tverdogo splava

AID 482-I

these tools. Detailed descriptions of each tool type are given, with instructions for design, and operation and practical use. The book contains data on the efficiency of the new tool designs in line production, and recommendations with reference to the operating conditions of these tools, as well as many illustrations, tables and diagrams. Of possible interest is the description of the electric spark technique on the OKB MSS single-circuit bench lathe used in the First State Bearing Plant im. Kaganovich (pp. 87-88, with illustrations).

Table of Contents

Foreword	PAGES
Introduction	#3
Ch. I Design of Tools with Hard-Alloy Multiple Blade Inserts	5-12
(Working principles; Shapes and sizes of inserts; Design of holders; ZIM type cutters; Design of milling cutters)	13-58
Ch. II Cutting Properties of Tools with Hard-Alloy Multiple Blade Inserts	59-79
(Cutters; Milling cutters)	
Ch. III Operation of Tools with Hard-Alloy Multiple Blade Inserts	80-89
(Preparing the inserts for the operation; Grinding the inserts)	

Pozbushchiye instrumenty s maogolezviyny  
vstavkami iz tverdogo splova

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PAGES

- Ch. IV Experience in Industrial Use of Tools with Hard-  
Alloy Multiple Blade Inserts 90-102
- Ch. V Efficiency of Use of Tools with Hard-Alloy  
Multiple Blade Inserts 103-109
- (Efficiency of use of: 1) cutters with prismatic inserts;  
2) ZIM cutters with inserted plates; 3) Face milling  
cutters with cylindrical inserts; Increased efficiency  
of tools with hollow inserts)

Purpose: The book is intended for engineers, technicians and Stakhanovites in machine-building plants.

Facilities: "Orgavtoprom" (Organization of the Automobile Industry)  
Institute; ZIM (Gor'kiy Automobile Plant im. Molotov); ZIS (Moscow  
Automobile Plant im. Stalin)

No. of Russian and Slavic References: None

Available: A.I.D., Library of Congress

3/3





1. FEL'DSHTEYN, Ya. I.; BOL'SHAKOV, V. M.; STIGNEYEV, Ya. F.
2. USSR (600)
4. Metal Cutting
7. Tools with removable hard-alloyed cutting bit. Stan. 1 instr. 23, No. 9, 1952.
9. Monthly List of Russian Accessions, Library of Congress, January 1953. Unclassified.

PHASE I

TREASURE ISLAND BIBLIOGRAPHICAL REPORT

AID 443 - I

BOOK

Call No.: TN731.P4

Author: FEL'DSHTEYN, E. I., Kand. of Tech. Sci.

Full Title: MACHINABILITY OF STEELS IN CONNECTION WITH THE CONDITIONS  
OF HEAT TREATMENT AND WITH THE MICROSTRUCTURE

Transliterated Title: Obrabatyvayemost' staley v svyazi s usloviyami  
termicheskoy obrabotki i mikrostrukturoy

Publishing Data

Originating Agency: None

Publishing House: State Scientific and Technical Publishing House of  
Literature on Mechanical Engineering and Shipbuilding ("Mashgiz")

Date: 1953

No. pp.: 255

No. of copies: 4,000

Editorial Staff

Editor: Klushin, M. I., Kand. of Tech. Sci.

Appraiser: Granovskii, G. I., Prof., Dr. of Tech. Sci.

The author dedicates this work to the staff of the Gor'kiy Automobile  
Plant im. V. M. Molotov and expresses his thanks to M. I. Klushin and  
Ya. F. Stigneyev, supervisors in the Laboratory of Metal Cutting, and  
to engineers and technicians in machine shops of this plant.

Text Data

Coverage: This book is the result of the author's ten-year investiga-  
tions of the machinability of structural and tool steels in relation  
to the conditions of heat treatment and to the microstructure. These

*Evaluation B-80557*

*1/6*

Obrabatyayemost' staley v svyazi s usloviyami  
termicheskoy obrabotki i mikrostrukturoy

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Investigations include the studies of the three basic factors of machinability: cutting speed, cleanness of finished surfaces and cutting pressure. Since the machinability of metals is not an abstract problem, it requires for its solution a wide range of experimental data. The main task of the author was not a simple gathering of information, but the establishment of general laws controlling these data, and their use for the practical needs of the industry. A specific feature of these investigations is the fact that they have been checked in industrial conditions. The author maintains that the correctness of the conclusions and their importance for the industry were proved by numerous tests and observations in machine shops of the Gor'kiy Automobile Plant.

Names of Russian scholars (since 1870) and of Soviet scientists (during the Stalin Five-Year Plans and in the postwar years), and discussions of their valuable contributions in this field are scattered through the book. Foreign scientists, particularly American and English, are mentioned with sharp criticism of their theories (e.g., p. 49-50). The book is provided with detailed descriptions of various kinds of steels, many illustrations of their microstructure and of the cleanness and roughness of surfaces, diagrams, temperature curves, numerous tables, sketches of machine elements, etc. The

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Obrabatyayemost' staley v svyazi s usloviyami  
termicheskoy obrabotki i mikrostrukturoy

AID 443 - I

work is based on a vast amount of literature (from 1870 to 1951).

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Foreword	PAGES
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Ch. I Combined Methods of Speedy Investigation of the Machinability of Metals	7
Test specimens and their utilization. Determination of the cutting speed and of the tool pressure. Investigations of the cleanness of finished surfaces.	14-23
Ch. II Effect of the Conditions of Heat Treatment and of the Microstructure of Steels on the Cutting Speed of Grinding (Experimental Data)	24-46
Medium-carbon structural steels (chrome steel 40X; Carbon steel 40; Chrome-manganese-silicon steel 35XGS). Low- carbon structural steel 15. High-carbon tool steel U12. High-speed steels.	
Ch. III Effect of the Machinability of Metals on the Wear of Cutting Tools	47-99
The temperature of cutting showing the machinability of metals in relation to cutting speeds. The abrasive properties	